

SIMULATION STUDY ON CONSTRUCTED RAPID INFILTRATION FOR TREATMENT OF SURFACE WASTEWATER IN TOWN

Zheng Yanxia¹, Feng Shaoyuan², Zhao Xuyang^{3,*}

¹ Zheng Yanxia, Doctor. Resource & Environment Department, Shijiazhuang College, Hebei 050035, P. R. China

² Feng Shaoyuan, professor. College of Water Conservancy & Civil Engineering, China Agricultural University, Beijing 100083, P. R. China

³ Zhao Xuyang, Professor. Resource & Environment Department, Shijiazhuang College, Hebei 050035, P. R. China

* Corresponding author, Address: Shijiazhuang College, Shijiazhuang, 050035, Hebei, P. R. China, Tel: 86-13931981959, Email: log2008@163.com

Abstract: On the base of land disposal, the objective of this study was to use constructed rapid infiltration (Abbreviation: CRI) to improve slightly polluted surface water in town. The data indicated that the average removal rates of BOD₅ and NH₄⁺-N were 80% and 65% in summer, respectively. In winter, the removal rates of BOD₅ decreased evidently with the lowering of water temperature, but the change of NH₄⁺-N was not obvious with the lowering of water temperature. The average removal rate of NH₄⁺-N was 60% in winter. The study results indicated that the constructed rapid infiltration system had better purification effect on the slightly polluted water. The system could still operate normally at low temperature in winter.

Keywords: Constructed Rapid Infiltration; Water temperature; Surface wastewater

1. INTRODUCTION

As an ecological treating technique, the land treatment systems are of good developing prospects because of its advantages, such as simple of facilities, economization of investment, convenience of operation, lower cost of energy and better effect of purgation. But it does still have some

problems. Among the problems, lower hydraulic loading and lower capability of treatment quantity per area were the most serious one. Constructed rapid infiltration was one kind of land treatment. It enhanced the hydraulic loading by replacing natural medium with artificial medium (Zhang et al., 2001, 2002; He 2001, 2005; Zheng, 2005). Buried sand-filter system and CRI system shared many similarities, such as filter velocity and the removal of particles, microorganisms, and biodegradable substances, but the hydraulic loading was slow, typically 0.2 meters per day (m/d) (Pauel et al., 1990; Markus et al., 1993; Andreas, 1997; Zhang et al., 2001). Some information about buried sand-filter may be helpful. In china, CRI system was developed in recent years, it was necessary to research more.

CRI system was utilized to improve the slightly polluted surface water; especially the application in the northern low-temperature area was studied rarely. For the feasibility of exploring CRI system to improve slightly polluted surface water, this paper developed Simulation experimental study on CRI system for BOD₅ and NH₄⁺-N removal effect under different seasons.

2. MATERIALS AND METHODS

2.1 Experimental apparatus

The experimental apparatus had been constructed and operated by the canal under the reservoir. Two replicates were performed per sand. Figure 1 is the sketch of the experimental apparatus of CRI system.

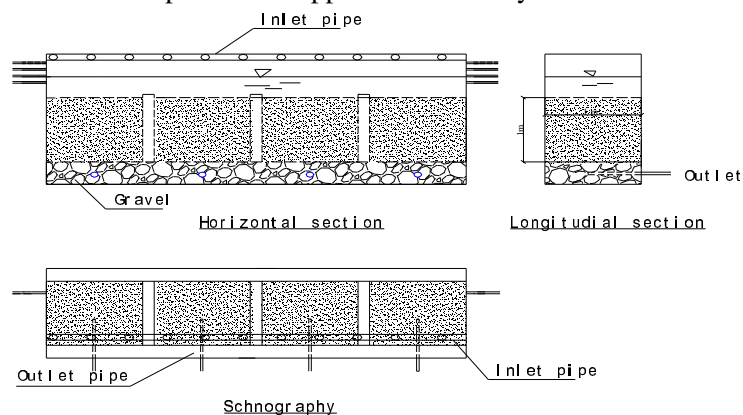


Figure1. The sketch of experimental CRI system

2.2 Porous media

Sand was used as porous media in the study. Mechanical composition of the two kinds of sand was described in Table 1. Two kinds of sand were not different obviously, were taken from the potential effluent recharge site in a river way.

Table 1. Mechanical composition of porous media

Size/mm					pH	Organic matter/%	CEC/ (cmol/kg)
10~2	2~0.5	0.5~0.25	0.25~0.075	<0.075			
5.26%	41.65%	39.91%	10.66%	2.73%	7.95	0.45	2.33
0%	47.26%	41.33%	9.61%	1.8%	7.8	0.52	2.2

2.3 Analytic methods of water quality

Influent water in this study was taken from surface wastewater in town. Parameters were determined by Environmental quality standard for surface water (State Environmental Protection Administration of China, GB 3838 - 2002).

3. RESULTS AND DISCUSSION

3.1 Water temperature on removal efficiency of BOD₅

Figure 2 showed effect of water temperature on removal of BOD₅. Removal of BOD₅ lowered with the decrease of water temperatures. The average removal rate of BOD₅ was 80% in summer with high temperature; in autumn with middle temperature and in winter with low temperature, the average removal rate of BOD₅ was 30%. Water temperature and removal rate of BOD₅ had similar trend of variation with a correlation coefficient of 0.9199.

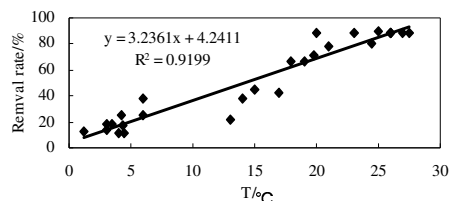


Figure 2. Effect of water temperature on removal of BOD₅

Basis on reaction formula equation, CRI system can be assumed as a plug flow reactor. That is, only in CRI system direction perpendicular to the flow

phenomena was mixed, and the flow direction was not mixed. Of course, this was an idealized model, but from a theoretical point of view, the analysis was feasible (Long, 2002). Figure 3 was Plug Flow Reactor Model.

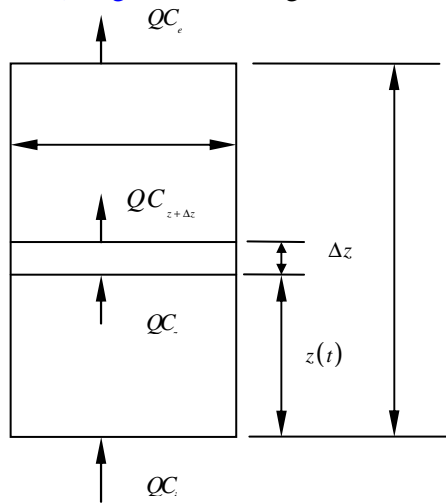


Figure 3. The sketch of Plug Flow Reactor Model

Calculated for energy conservation in $A\Delta z$:

$$QC_z + (A\Delta z)r = QC_{z+\Delta z} + (A\Delta z)(dC_z / dt) \quad (1)$$

Where : Q is flow. C_z is concentration. r is reaction rate

Ordered $\Delta z \rightarrow dz$, Equation (1) can be written :

$$-(Q/A)(dC_z / dz) + r = dC_z / dt \quad (2)$$

Where Q/A can be used to replace by U , and z/U can be used to replace by θ , omitted subscript z , equation (2) can be written :

$$-(dC / d\theta) + r = dC / dt \quad (3)$$

In steady state, $dC / dt = 0$:

$$dC / d\theta = r \quad (4)$$

Due to the low concentration, the removal rate followed the first-order reaction formula :

$$r = -kC \quad (5)$$

Where : k is reaction rate constant.

Put equation(5)into equation(4), and integration :

$$C = C_i \exp(-k\theta) \quad (6)$$

On both sides of equation (6) with log :

$$\ln(C_i / C) = k\theta \quad (7)$$

Basis on the concentration of BOD₅, the approximation of reaction rate k can be drawn in CRI system. k was a coefficient with water temperature. Such as BOD₅, $K_{20^\circ\text{C}}/K_{25^\circ\text{C}}$ was 0.94, and $K_{10^\circ\text{C}}/K_{15^\circ\text{C}}$ was 0.48, and $K_{15^\circ\text{C}}/K_{20^\circ\text{C}}$ was 0.93. These indicated reaction rate decreased 6%, when water temperature was dropped from 25°C to 20°C; Reaction rate decreased 7%, when water temperature decreased from 20°C to 15°C; reaction rate decreased 52%, when water temperature decreased from 15°C to 10°C .These suggested water temperature more low; reaction rate decreased the proportion more big. This accorded with the experimentation result that the effect of change of water temperature was little in high temperature stage, but in low temperature stage, the effect was obvious.

3.2 Water temperature on removal efficiency of NH₄⁺-N

Figure 4 showed effect of water temperature on removal of NH₄⁺-N. Removal of NH₄⁺-N was not obvious with the change of water temperature. But the trend was increased with the increasing of water temperature. Firstly, NH₄⁺-N was adsorbed into the infiltration media and happened nitrification. Because NH₄⁺-N was biochemical substances, it was totally absorbed by microorganism. So the removal rates of NH₄⁺-N were more constant than on the removal of organic matter. Even in the low temperature close to 0°C, the ammonia removal rate remained at 45%. Therefore, CRI system had a certain removal effect on NH₄⁺-N in slightly polluted water under low temperatures.

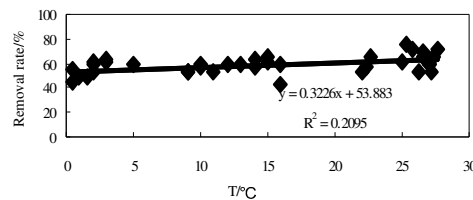


Figure 4. Effect of water temperature on removal of NH₄⁺-N

Basis on reaction formula equation, the lower of $\text{NH}_4^+\text{-N}$ removal rate indicated the lower of $\text{NH}_4^+\text{-N}$ removal speed in CRI system. Therefore, Monod kinetic equation was used to note ammonia oxidation reaction (Gu, 1993).

Basis on Monod equation :

$$\mu_{NS} = (\mu_{\max})_{NS} N / (K_N + N) \quad (8)$$

Where : μ_{NS} is growth rate of nitrosobacteria (min^{-1}). $(\mu_{\max})_{NS}$ is max growth rate of nitrosobacteria (min^{-1}). N is concentration of $\text{NH}_4^+\text{-N}$ (mg/L). K_N is saturation constant (mg/L, $K_N = 10^{0.051T-1.158}$). T is temperature ($^{\circ}\text{C}$).

$$(dX/dt)/X = -y_0 (dN/dt)/X \quad (9)$$

$$\mu_{NS} = (dX/dt)/X \quad (10)$$

$$v = -(dN/dt)/X \quad (11)$$

$$\therefore \mu_{NS} = y_0 v \text{ or } (\mu_{\max})_{NS} = y_0 v_{\max} \quad (12)$$

Where : X is concentration of nitrosobacteria (mg/L). y_0 is yield (mg Nitrosobacteria / mg $\text{NH}_4^+\text{-N}$). v is removal speed of $\text{NH}_4^+\text{-N}$ (min^{-1}). v_{\max} is max removal speed of $\text{NH}_4^+\text{-N}$ (min^{-1}).

Put equation(12) into equation(10) :

$$v = v_{\max} N / (K_N + N) \quad (13)$$

In the wastewater treatment process, removal of the pollutants was major, and microbial growth was the result of pollutants removal. Therefore, equation (13) was more practical.

Assumed :

(1) The nitrosobacteria concentration of entrance was similar to the concentration of exports in CRI system. At this point, the nitrosobacteria concentration can be said that the average concentration X_a .

(2) The using speed of $\text{NH}_4^+\text{-N}$ was same to the reducing speed of $\text{NH}_4^+\text{-N}$ concentration along the water flow direction.

So :

$$v = -(dN/dt)/X_a = v_{\max} N / (K_N + N) \quad (14)$$

Arranged :

$$K_N dN + NdN = -v_{\max} X_a N dt \quad (15)$$

Integral :

$$(N_i - N_e) + K_N \ln(N_i/N_e) = v_{\max} X_a t \quad (16)$$

Ordered $V_{\max} = v_{\max} X_a$, called the max removal rate (mg/L•min) :

$$(N_i - N_e) + K_N \ln(N_i/N_e) = V_{\max} t \quad (17)$$

Where : N_i is concentration of NH_4^+ -N of entrance (mg/L). N_e is concentration of NH_4^+ -N of exports(mg/L).

Basis on the concentration of NH_4^+ -N, the approximation of max removal speed V_{\max} can be drawn in CRI system. V_{\max} was a coefficient with water temperature. Such as NH_4^+ -N, $V_{\max(5^\circ\text{C})}/V_{\max(10^\circ\text{C})}$ was 0.65, and $V_{\max(0.5^\circ\text{C})}/V_{\max(5^\circ\text{C})}$ was 0.525. This indicated max removal speed decreased 35%, when water temperature was dropped from 10°C to 5°C ; The max removal speed decreased 47.5%, when water temperature decreased from 5°C to 0.5°C. Removal efficiency of NH_4^+ -N was not significantly different with the increase of water temperatures. The average removal rate of NH_4^+ -N was 65% in summer with high temperature, in autumn with middle temperature and in winter with low temperature. The changes of NH_4^+ -N were not obvious with the lowering of water temperature.

CRI system had better removal effect on NH_4^+ -N in slightly polluted water, but water temperature had not obvious effect on removal effect. This suggested that nitrobacteria and nitrosomonas adapted to low temperature (Wang et al., 1999; Zhou et al., 2000). Therefore, CRI system had a certain removal effect on NH_4^+ -N in slightly polluted water under low temperatures.

4. CONCLUSIONS

(1)CRI system had a significant removal effect on slightly polluted surface water. The simulation experiment indicated that the average removal rates of BOD_5 and NH_4^+ -N were 80% and 65% in summer with high temperature, respectively. The average removal rates of BOD_5 and NH_4^+ -N were 30% and 60% in winter with low temperature, respectively

(2)Removal of BOD_5 was lowered with the lowering of water temperature. In winter, the removal rates of BOD_5 lowered evidently with

the lowering of water temperature, but the change of $\text{NH}_4^+\text{-N}$ was not obvious with the lowering of water temperature.

(3)The removal efficiency decreased with the lowering of water temperature. This suggested that microbial activity decreased with the lowering of water temperature. The lower water temperature, microbial activity was affected greater. In winter, the CRI system should take measures to keep from freeze. The system could operate normally at low temperature in winter.

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